

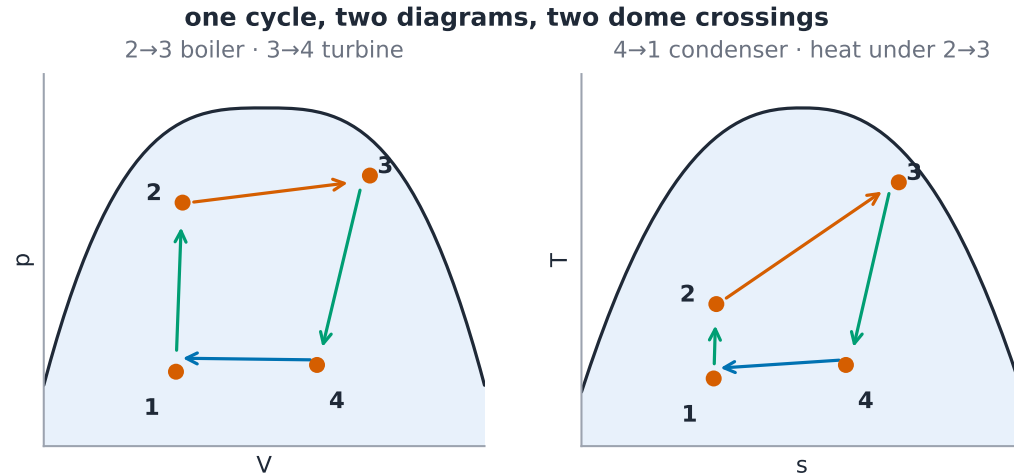
Exercise walk-through

5.5

Power cycles

University Mechanical Engineering

Power cycles: the Rankine baseline



Boiler 4 MPa, condenser 10 kPa: $x_4 = \mathbf{0.7227}$, turbine 880.3, pump 4.0, heat in 2605.6 kJ/kg - $\eta = \mathbf{33.6\%}$. Superheat: $\eta = \mathbf{39.1\%}$, $x_4 = \mathbf{0.8157}$; reheat keeps the exhaust dry.

Exercises 2.1-2.2

2.1 For this cycle – boiler at 8 MPa giving saturated vapour with $h_3 = 2750.0$ kJ/kg and $s_3 = 5.750$ kJ/(kg K); condenser at 20 kPa with $h_f = 250.0$, $h_{fg} = 2350.0$ kJ/kg, $s_f = 0.830$, $s_{fg} = 7.070$ kJ/(kg K); pump inlet $h_1 = 250.0$ kJ/kg with $v_f = 0.001020$ m³/kg – the turbine exit quality (four decimals) and exit enthalpy (one decimal, kJ/kg). [4]

2.2 For the cycle of 2.1: the turbine work and the pump work (one decimal each, kJ/kg). [3]

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2.1

- $x_4 = (s_3 - s_f)/s_{fg} = (5.750 - 0.830)/7.070 = \mathbf{0.6959}$.
- $h_4 = 250.0 + 0.6959 \times 2350.0 = \mathbf{1885.4}$ kJ/kg.

2.2 For the cycle of 2.1: the turbine work and the pump work (one decimal each, kJ/kg). [3]

2.2

- $w_t = h_3 - h_4 = 2750.0 - 1885.4 = \mathbf{864.6}$ kJ/kg.
- $w_p = v_f \Delta p = 0.001020 \times 7980 = \mathbf{8.1}$ kJ/kg.

Exercises 2.3-2.4

2.3 For the cycle of 2.1: the heat input per kilogram (one decimal, kJ/kg) and the cycle thermal efficiency (one decimal, percent). [3]

2.4 One sentence each: why does raising the boiler pressure raise the efficiency, and why must the exhaust quality be watched even when the arithmetic is clean? [4]

Exercises 2.3-2.4

2.3 For the cycle of 2.1: the heat input per kilogram (one decimal, kJ/kg) and the cycle thermal efficiency (one decimal, percent). [3]

2.3

- $h_2 = 250.0 + 8.1 = 258.1$, so $q_{in} = 2750.0 - 258.1 = \mathbf{2491.9}$ kJ/kg.
- $\eta = (864.6 - 8.1)/2491.9 = 856.5/2491.9 = \mathbf{34.4\%}$.

2.4 One sentence each: why does raising the boiler pressure raise the efficiency, and why must the exhaust quality be watched even when the arithmetic is clean? [4]

2.4

- Higher boiler pressure raises the average temperature of heat addition, so the second-law ceiling $1 - T_{out}/T_{in,avg}$ rises while the pump cost grows only as $v \Delta p$.
- Wet exhaust erodes the last-stage blades: x_4 below roughly 0.88 ruins the machine even when the cycle balances - superheat and reheat exist to keep it dry.