

5.7 Frequency response of amplifiers

Name: _____ Class: _____ Date: _____

Total: 20 marks

KEY WORDS coupling capacitor • Miller capacitance • dominant pole

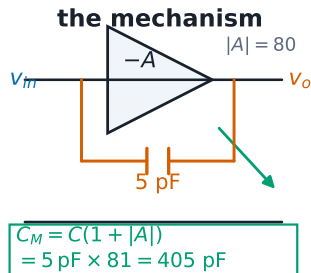
Objective

Locate low- and high-frequency corners from coupling capacitors and internal poles, apply the Miller multiplication, and compute bandwidth and gain-bandwidth limits – each corner checked against its own RC.

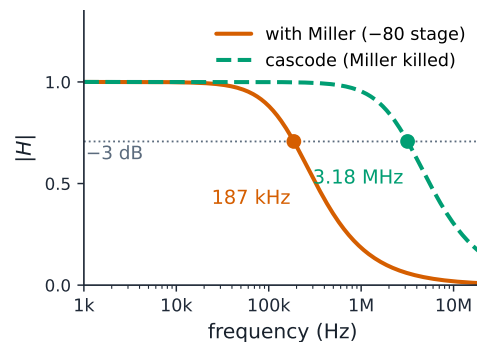
1 Key knowledge and worked examples

■ Two families of corner

Coupling capacitors (series, between stages) set the LOW corner $f_L = 1/(2\pi RC)$ per stage – the total low corner is the quadrature sum of stage corners. Internal capacitances set the HIGH corner via the **domant pole** : $f_H \approx 1/(2\pi R_{eq} \cdot C_{eq})$ at the input node.



what it costs (and the cascode cure: 17×)



The Miller multiplication and the bandwidth it costs; the cascode reclaims 17×.

■ Worked example: Miller multiplication

A stage with gain -80 has $C_{gb} = 5 \text{ pF}$ base-to-collector. The input sees the **Miller capacitance** $C_M = C_{gb}(1 + |A_v|) = 5 \text{ p} \times 81 = 405 \text{ pF}$. With $R_{eq} = 2 \text{ k}\Omega$ and 20 pF stray: $f_H = 1/(2\pi \times 2000 \times 425 \text{ p}) = 187 \text{ kHz}$. The Miller effect explains why high-gain stages roll off first – and why the cascode (which holds the collector nearly still, killing the gain across C_{gb}) extends bandwidth for free.

■ Gain-bandwidth closure

For an op-amp stage, once f_H is known, the **gain-bandwidth product** closes the design: gain $\times$ bandwidth = constant. A discrete stage's own corners multiply the same way – two cascaded stages each -3 dB at a frequency give -6 dB total there, and the composite -3 dB point is lower than either.

2 Practice

2.1 A coupling capacitor $10 \text{ }\mu\text{F}$ into a $15 \text{ k}\Omega$ input resistance: compute f_L . [2]

2.2 An input node with $R_{eq} = 4 \text{ k}\Omega$ and $C_{eq} = 50 \text{ pF}$: compute f_H . [2]

2.3 A stage of gain -50 has 4 pF across it: compute the Miller capacitance the input sees. [2]

3 Exam-style questions

3.1 A single-stage CE amplifier has: input coupling $2.2\ \mu\text{F}$ into a $20\ \text{k}\Omega$ total resistance; a bypass capacitor $47\ \mu\text{F}$ looking into $R_E \parallel (r_\pi / (\beta + 1)) \approx 25\ \Omega$; and a high-frequency node of $R_{eq} = 1.5\ \text{k}\Omega$ with $C_{gb} = 4\ \text{pF}$ at stage gain -60 plus $25\ \text{pF}$ stray.

Compute each low corner (coupling, bypass) and the high corner (with Miller); state the amplifier's passband edges; and compute the bypass capacitor needed to push ITS corner a decade below the coupling corner. [7]

3.2 A two-stage amplifier has each stage at gain -40 with input $R_{eq} = 2\ \text{k}\Omega$, $C_{gb} = 5\ \text{pF}$, stray $20\ \text{pF}$.

Compute each stage's Miller capacitance and f_H ; compute the composite $-3\ \text{dB}$ high corner of the cascade (quadrature combination: $1/f_{\text{total}}^2 \approx 1/f_1^2 + 1/f_2^2$ for two identical stages – equivalently $f_{\text{total}} = f_H \cdot \sqrt{2^{1/2} - 1}^{1/2} = 0.644\ f_H$); and state the gain-bandwidth product of one stage. Verify the composite against the per-stage corner. [7]
