

# 11.1 Rotation, buoyancy and terminal-speed balances

Name: \_\_\_\_\_ Class: \_\_\_\_\_ Date: \_\_\_\_\_

Total: 10 marks

KEY WORDS moment of inertia • terminal speed

## Objective

Use pivot torque and rotational inertia consistently; Partition rolling kinetic energy with the no-slip constraint; Balance buoyancy and drag for composite bodies. Original public practice; not an ETS paper.

## 1 Key knowledge and worked examples

About a fixed pivot, torque is  $r \times F$ . A uniform rod pivoted at one end has  $I = ML^2/3$ ; gravity acts at  $L/2$ . With angle  $\theta$  from vertical, torque magnitude is  $Mg(L/2)\sin\theta$ , giving angular-acceleration magnitude  $3g \sin\theta/(2L)$ . Define direction separately; centre-of-mass inertia needs a parallel-axis correction.

No-slip rolling gives  $v = R\omega$ . With  $I = \beta MR^2$ ,  $K = \frac{1}{2}Mv^2(1 + \beta)$  and the rotational fraction is  $\beta/(1 + \beta)$ . Disk:  $1/3$ ; sphere:  $2/7$ ; hoop:  $1/2$ . Static friction can provide torque without dissipating energy at a stationary contact on a fixed surface.

Floating composites displace enough fluid to balance total weight. If submerged wood fraction is  $f$  with a stone dry, then putting stone volume  $V_s$  fully underwater reduces the wood fraction to  $f - V_s/V$ . The stone retains its weight while adding buoyancy; check that flotation/orientation assumptions are possible.

Terminal speed is a force balance. For quadratic drag  $Cv^2$  and negligible buoyancy,  $v_t = \sqrt{Mg/C}$ . Identical shapes share  $C$ , so a mass ratio  $r$  gives speed ratio  $\sqrt{r}$ . With buoyancy use effective weight; linear drag gives a different scaling. Terminal motion has nonzero balancing forces.

### ■ Worked method

A body rolls without slipping on a fixed surface. The no-slip constraint is  $v = R\omega$ .

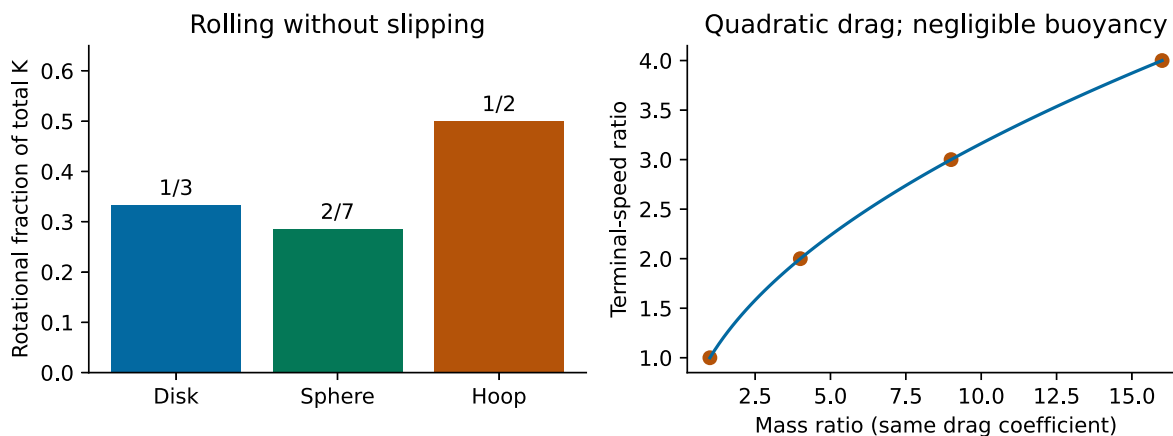
$$K = \frac{1}{2}Mv^2 + \frac{1}{2}I\omega^2 = \frac{1}{2}Mv^2(1 + \beta), \quad I = \beta MR^2.$$

For a solid disk,  $\beta = 1/2$ , so the rotational share is

$$\frac{K_{rot}}{K} = \frac{\beta}{1 + \beta} = \frac{1/2}{3/2} = \frac{1}{3}.$$

For a uniform rod pivoted at one end, use  $I = ML^2/3$ , not its centre-of-mass inertia. About this pivot  $\tau = -Mg(L/2) \sin \theta$ , for theta measured from downward vertical.

$$\ddot{\theta} = \tau/I = -3g \sin \theta/(2L).$$



## 2 Practice

**2.1** Choose one answer. For a uniform rod pivoted at one end, gravitational angular-acceleration magnitude at angle  $\theta$  from vertical is: [1]

- A  $g \sin \theta / L$
- B  $3g \sin \theta / (2L)$
- C  $3g \cos \theta / (2L)$
- D  $6g \sin \theta / L$
- E  $g / (2L)$

**2.2** Choose one answer. For a solid sphere  $I = 2MR^2/5$  rolling without slipping, the rotational fraction of total K is: [1]

- A  $2/5$
- B  $1/2$
- C  $2/7$
- D  $5/7$
- E  $1/5$



## Solutions

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**2.1 B** Divide  $Mg(L/2)\sin\theta$  by  $ML^2/3$ .

Compare the rejected options:  $g \sin\theta/L$ ;  $3g \cos\theta/(2L)$ ;  $6g \sin\theta/L$ ;  $g/(2L)$ . Use the stated model and conditions.

**2.2 C** Use  $\beta/(1+\beta)=(2/5)/(7/5)=2/7$ .

Compare the rejected options:  $2/5$ ;  $1/2$ ;  $5/7$ ;  $1/5$ . Use the stated model and conditions.

**2.3 3.** The ratio is  $\sqrt{9}$ .

**2.4 False.** Drag balances the effective weight; it is generally nonzero.

**3.1** Energy gives  $Mgh = \frac{1}{2}Mv^2(1+2/5)$ , hence  $v = \sqrt{10gh/7}$ . The slider has  $v_s = \sqrt{2gh}$ , so  $v/v_s = \sqrt{5/7} < 1$ . Slipping breaks  $v = R\omega$  and can dissipate energy through kinetic friction. Award energy relation, speed, comparison and the constraint/loss distinction.